

## IN THE CLAIMS

Claims 1-25 (canceled)

26. (new) A process for producing a polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner and comprises inorganic particles, on a substrate that comprises metal, said substrate optionally being precoated on at least one side of the substrate, e.g. with at least one zinc layer or/and a zinc-containing alloy layer or/and with at least one pretreatment layer, wherein

a lacquer-like mixture comprising resin and inorganic particles is applied to an optionally precoated substrate and is optionally dried and at least partly crosslinked,

wherein the mixture comprises at least 10 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, and

wherein these electrically conductive particles have a steep particle size distribution,

in which the transfer value  $d_{99}$  relative to the transfer value  $d_{10}$  in the volume plot has a factor of at most 10 and

in which 3 to 22 vol.% of the electrically conductive particles, measured with a Mastersizer 2000 with a Hydro 2000S measuring head from Malvern Instruments, in a volume plot are larger than the average layer thickness of the dried and optionally also cured coating, determined on scanning electron microscopy photographs,

wherein this coating has a thickness of less than 10  $\mu\text{m}$ ,

wherein a small content of over-sized particles of electrically conductive particles projects out of the polymeric coating like antennae and

wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5.

27. (new) A process for producing a polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner and comprises inorganic particles, on a substrate that comprises metal, it being possible for the substrate optionally to be precoated on at least one side of the substrate, e.g. with at least one zinc layer or/and a zinc-containing alloy layer or/and with at least one pretreatment layer, wherein

a lacquer-like mixture comprising resin and inorganic particles is applied to an optionally precoated substrate and is optionally dried and at least partly crosslinked,

wherein the mixture comprises at least 10 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, and

wherein the envelope curve of the particle size distribution for these electrically conductive particles, measured with a Mastersizer 2000 with a Hydro 2000S measuring head from Malvern Instruments, in a logarithmic volume plot is at least twin-peaked and is divided into individual Gauß distribution curves,

wherein a first minimum of the individual Gauß distribution curves between the main peak and the next larger peak of these distribution curves, determined in  $\mu\text{m}$ , is greater by a factor of 0.9 to 1.8 than the average dry film thickness of the dried and optionally also cured coating, determined on scanning electron microscopy photographs,

but wherein not more than 22 vol.% of the particle size distribution of these electrically conductive particles is larger than the average dry film thickness

wherein this coating has a thickness of less than 10  $\mu\text{m}$ ,

wherein a small content of over-sized particles of electrically conductive particles projects out of the polymeric coating like antennae and

wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5.

28. (new) The process according to claim 26, wherein the particle size distribution of the remaining inorganic particles, i.e. of all the inorganic particles without the electrically conductive particles, measured with a Mastersizer 2000 with a Hydro 2000S measuring head from Malvern Instruments, has a higher volume content of the largest particles at the particle volume transfer value  $d_{98}$  or in the Gauß distribution curve with the largest particle volumes than at the particle volume transfer value  $d_{98}$  or in the corresponding Gauß distribution curve of the electrically conductive particles.

29. (new) The process according to claim 26, wherein the mixture comprises no electrically conductive particles having a particle size diameter greater than five times the value of the average dry film thickness of the dried and optionally also cured coating.

30. (new) The process according claim 26, wherein the mixture comprises 20 to 80 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture.

31. (new) The process according to claim 26, wherein the mixture additionally comprises very soft or soft particles which are capable of sliding, such as e.g. graphite, molybdenum disulfide, carbon black or/and zinc or corrosion protection pigment(s).

32. (new) The process according to claim 26, wherein the electrically conductive particles are chosen from particles based on alloys, boride, carbide, oxide, phosphide, phosphate, silicate and silicide, preferably chosen from alloys, carbides, oxides and phosphides.

33. (new) The process according to claim 26, wherein the mixture additionally comprises at least one resin and optionally at least one curing agent, at least one photoinitiator, at least one additive, water or/and an organic solvent and optionally 0.5 to 15 wt.% of corrosion protection pigment(s).

34. (new) The process according to claim 26, wherein the very soft or soft particles which are capable of sliding, such as e.g. graphite, are in each case not ground or are ground with only a low intensity before addition to the mixture or in the mixture or/and in a portion of the mixture.

35. (new) The pccording to claim 26, wherein electrically conductive particles are ground separately and, where appropriate, mixed with similar batches of electrically conductive particles.

36. (new) The process according to claim 26, wherein on grinding of the electrically conductive particles, the over-sized particles are predominantly comminuted, so that a narrower particle size distribution arises.

37. (new) The process according to claim 26, wherein the curing agent of at least one is added in an excess relative to the amount of binder of the mixture which is to be crosslinked with this.

38. (new) The process according to claim 26, wherein the mixture applied to the substrate is dried, stoved, irradiated with free radicals or/and heated in order to form a thoroughly crosslinked, corrosion-resistant, viscoelastic coating.

39. (new) The process according to claim 26, wherein a coating having a thickness of less than 8  $\mu\text{m}$ , preferably less than 6  $\mu\text{m}$  and particularly preferably of less than 4  $\mu\text{m}$ , measured in the dry state on scanning electron microscopy photographs, is produced.

40. (new) The process according to claim 26, wherein the mixture is free or substantially free from organic lubricants, such as e.g. based on PTFE, silicone or oil, inorganic or/and organic acids or/and heavy metals and other cations, such as arsenic, lead, cadmium, chromium, cobalt, copper or/and nickel.

41. (new) The process according to claim 33, wherein the substrate comprises at least one metal or/and at least one alloy and is optionally precoated, in particular comprises a strip or sheet comprising aluminium, an aluminium, iron or magnesium alloy or steel, such as e.g. automobile steels.

42. (new) The process according to claim 33, wherein the mixture according to the invention is applied directly to a pretreatment coating.

43. (new) The process according to claim 27, wherein the particle size distribution of the remaining inorganic particles, i.e. of all the inorganic particles without the electrically conductive particles, measured with a Mastersizer 2000 with a Hydro 2000S measuring head from Malvern Instruments, has a higher volume content of the largest particles at the particle volume transfer value  $d_{98}$  or in the Gauß distribution curve with the largest particle volumes than at the particle volume transfer value  $d_{98}$  or in the corresponding Gauß distribution curve of the electrically conductive particles.

44. (new) The process according to claim 27, wherein the mixture comprises no electrically conductive particles having a particle size diameter greater than five times the value of the average dry film thickness of the dried and optionally also cured coating.

45. (new) The process according to claim 27, wherein the mixture comprises 20 to 80 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture.

46. (new) The process according to claim 27, wherein the mixture additionally comprises very soft or soft particles which are capable of sliding, such as e.g. graphite, molybdenum disulfide, carbon black or/and zinc or corrosion protection pigment(s).

47. (new) The process according to claim 27, wherein the electrically conductive particles are chosen from particles based on alloys, boride, carbide, oxide, phosphide, phosphate, silicate and silicide, preferably chosen from alloys, carbides, oxides and phosphides.

48. (new) The process according to claim 27, wherein the mixture additionally comprises at least one resin and optionally at least one curing agent, at least one photoinitiator, at least one additive, water or/and an organic solvent and optionally 0.5 to 15 wt.% of corrosion protection pigment(s).

49. (new) The process according to claim 27, wherein the very soft or soft particles which are capable of sliding, such as e.g. graphite, are in each case not ground or are ground with only a low intensity before addition to the mixture or in the mixture or/and in a portion of the mixture.

50. (new) The process according to claim 27, wherein electrically conductive particles are ground separately and, where appropriate, mixed with similar batches of electrically conductive particles.

51. (new) The process according to claim 27, wherein on grinding of the electrically conductive particles, the over-sized particles are predominantly comminuted, so that a narrower particle size distribution arises.

52. (new) The process according to claim 27, wherein the curing agent of at least one is added in an excess relative to the amount of binder of the mixture which is to be crosslinked with this.

53. (new) The process according to claim 27, wherein the mixture applied to the substrate is dried, stoved, irradiated with free radicals or/and heated in order to form a thoroughly crosslinked, corrosion-resistant, viscoelastic coating.

54. (new) The process according to claim 27, wherein a coating having a thickness of less than 8  $\mu\text{m}$ , preferably less than 6  $\mu\text{m}$  and particularly preferably of less than 4  $\mu\text{m}$ , measured in the dry state on scanning electron microscopy photographs, is produced.

55. (new) The process according to claim 27, wherein the mixture is free or substantially free from organic lubricants, such as e.g. based on PTFE, silicone or oil, inorganic or/and organic acids or/and heavy metals and other cations, such as arsenic, lead, cadmium, chromium, cobalt, copper or/and nickel.

56. (new) The process according to claim 48, wherein the substrate comprises at least one metal or/and at least one alloy and is optionally precoated, in particular comprises a strip or sheet comprising aluminium, an aluminium, iron or magnesium alloy or steel, such as e.g. automobile steels.

57. (new) The process according to claim 48, wherein the mixture according to the invention is applied directly to a pretreatment coating.

58. (new) A polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner and comprises inorganic particles, on a thin strip, on a metallic sheet or on another type of metallic body as the substrate, wherein the mixture for producing the coating comprises at least 10 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5, wherein the coating has an average dry film thickness of less than 10  $\mu\text{m}$ , and wherein the substrate coated in this manner leads to an abrasion only of less than 2 g per  $\text{m}^2$  during severe shaping or severe pressing in a die of a large press.

59. (new) A polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner, comprises inorganic particles and has an average dry film thickness of at least 4  $\mu\text{m}$  and less than 10  $\mu\text{m}$ , on a thin metallic strip, on a metallic sheet or on another type of metallic body as the substrate, wherein the mixture for producing the coating comprises at least 10 wt.% of electrically conductive particles having an electrical conductivity better than that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5, and wherein by resistance spot welding at least 1,000 welding points, can be set through two substrates coating in this manner under very difficult welding conditions such as are currently conventional in the automobile industry, without replacement or reworking of the welding electrodes and without troublesome smoke traces.



60. (new) A polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner, comprises inorganic particles and has an average dry film thickness of at least 4  $\mu\text{m}$  and less than 10  $\mu\text{m}$ , on a strip or a sheet of steel 0.8 mm thick, precoated on both sides in each case with at least one layer of zinc or of a zinc-containing alloy and optionally with at least one pretreatment coating, wherein by resistance spot welding at least 1,000 welding points, can be set through two substrates coating in this manner under very difficult welding conditions such as are currently conventional in the automobile industry, without replacement or reworking of the welding electrodes and without troublesome smoke traces, the coating having been produced using a mixture which comprises at least 10 wt.% of electrically conductive particles having an electrically conductivity better than that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5.

61. (new) A polymeric, corrosion-resistant, electrically conductive and electrically weldable coating, which can be shaped in a low-abrasive manner, comprises inorganic particles and has an average dry film thickness of at least 2  $\mu\text{m}$  and less than 10  $\mu\text{m}$ , on a strip or a sheet 0.8 mm thick of steel, precoated on both sides in each case with at least one layer of zinc or of a zinc-containing alloy and optionally with at least one pretreatment coating, wherein by resistance spot welding at least 1,800 welding points, can be set through two substrates coating in this manner under very difficult welding conditions such as are currently conventional in the automobile industry, without replacement or reworking of the welding electrodes and without troublesome smoke traces, the coating having been produced using a mixture which comprises at least 10 wt.% of electrically conductive particles having an electrically conductivity better than

that of particles of pure zinc and having a Mohs hardness of greater than 4, based on the solids contents of the mixture, wherein at least some of the electrically conductive particles have a Mohs hardness of at least 5.5.

62. (new) A polymeric, electrically conductive and electrically weldable coating, which comprises inorganic particles and can be shaped in a low-abrasive manner, on a substrate, which is produced by the process according to one of claim 26.

63. (new) A composition comprising steel which is sensitive to bake-hardening and at least one coating produced according to the process of claim 26 with thermal curing at temperatures not above 160 °C.

64. (new) A polymeric, electrically conductive and electrically weldable coating, which comprises inorganic particles and can be shaped in a low-abrasive manner, on a substrate, which is produced by the process according to one of claim 27.

65. (new) A composition comprising steel which is sensitive to bake-hardening and at least one coating produced according to the process of claim 27 with thermal curing at temperatures not above 160 °C.